

Black building profiles according to DIN 7863 and RAL-GZ 716/1 Alternatives to carbon black: Aktisil VM 56

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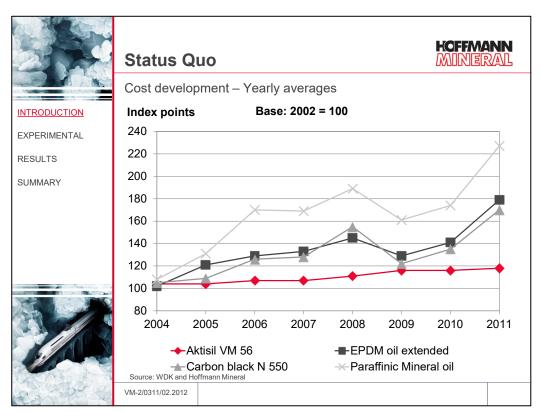
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1 Introduction

Typical formulations for black window sections and glazing profiles are based on EPDM, carbon black and paraffinic mineral oil. This means the major part of the raw materials is petroleum based (*Table 1 and fig. 4*).

According to the crude oil price, the raw material prices are subject to considerable variations. The long term trend is clearly pointing upwards (*Fig. 1*).

The price of mineral fillers is only marginally affected by the crude oil price; over the long term there will be a slight increase, and this without big variations (*Fig. 1*).





As evident from *Figure 2*, it is hardly possible to obtain at equal hardness a further cost reduction via the carbon black and plasticizer loading. As a cost optimized starting point, a carbon black / plasticizer loading of 180 / 80 phr was selected.

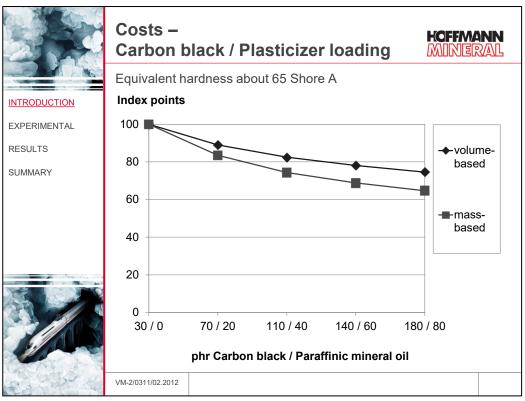


Fig. 2

	Objective	•	MINIERAL		
INTRODUCTION EXPERIMENTAL		strate an alternative formulation appr petroleum based raw materials.	roach in order to		
RESULTS		 As a cost optimized starting point, a formulation with a carbon black / plasticizer loading of 180 / 80 phr was selected. 			
SUMMARY	 As guidelines were the mechanical requirements of the German standard DIN 7863 and RAL-GZ 716/1. 				
	• Calcium carbonate represents the traditional cost reducing filler, but at high loadings it does not impart sufficiently high mechanical properties.				
		t, <mark>Aktisil VM 56</mark> even at high loadings hanical results along with very g			
	VM-2/0311/02.2012				

Fig. 3

2.1 Compound Formulation

A typical formulation for black window sections and glazing profiles is based on EPDM, carbon black and paraffinic plasticizer oil. This way, the major portion for the raw materials is petroleum based, as is clearly visible in *Figures* 4 - 6.

	Base Formulation	HOFFMANN		
	EPDM – 65 Shore A			
INTRODUCTION		phr		
EXPERIMENTAL	Keltan 8340 A	100.0		
RESULTS	PEG 4000	2.0		
SUMMARY	Processing aid	3.0		
	Carbon black N 550	180.0		
	Paraffinic mineral oil, Plasticizer	80.0		
	Calcium oxide	10.0		
	TAC GR 50 %	3.0		
	Perkadox 14/40 pd	8.0		
	Total	386.0		
AS STAR	VM-2/0311/02.2012			

Table 1

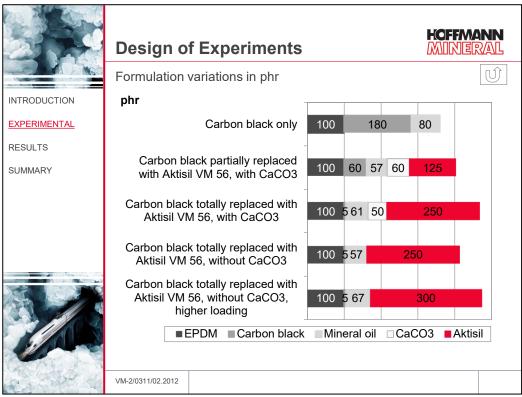


Fig. 4

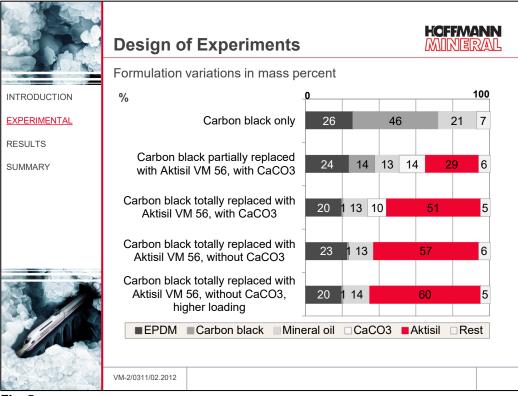


Fig. 5

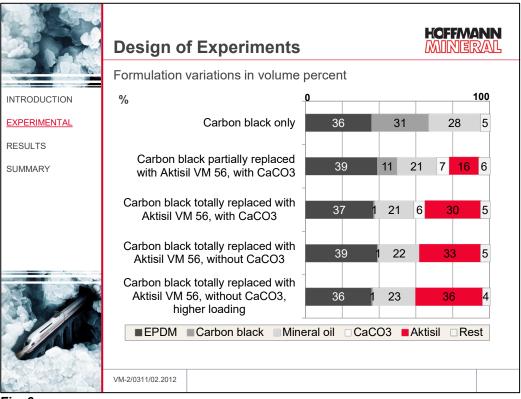


Fig. 6

The petroleum based raw materials are shown in different red shades. As evident from *Figures 4 – 6*, the portion of petroleum based raw materials is decreasing with an increasing part of mineral fillers, which are shown in green and yellow. As a result, the variations of compound costs caused by crude oil price changes are minimized.

The typical conventional filler is carbon black N 550. In order to achieve a closer price control, the carbon black is replaced by calcium carbonate and Aktisil VM 56. As evident from the levels of oil number, specific surface area BET and DBP absorption, the carbon black is distinguished by a markedly higher surface area and structure compared to the calcium carbonate. Aktisil VM 56 presents itself within these extremes. In order to obtain an equivalent hardness of the compounds, the replacement loading had to be adjusted at appr. 1:2 phr (*Table 2 and fig. 4*).

	Fillers, Characteristics				HOFFMANN MINERAL		
			Carbon black N 550	Calcium- carbonat surface treated	Aktisil VM 56		
RESULTS	Density	[g/cm ³]	1.8	2.7	2.6		
SUMMARY	Particle size d ₅₀	[µm]		2.7	2.0		
	Particle size d ₉₇	[µm]		25	9		
	Sieve residue >40 µm	[mg/kg]	= 300</td <td>14</td> <td>4</td>	14	4		
	Sieve residue 45 µm (Siev No. 325)		10				
	Oil absorption	[g/100g]		19	50		
	DBP absorption	[ml/100 g]	121				
	Specific surface area BET	[m²/g]	41	2.1	11		
	CTAB Surface area	[m²/g]	42				
	Surface treatment	none	Stearate	vinyl functionalized			
	VM-2/0311/02.2012						

Table 2

2.2 Compounding and Curing

All compounds were mixed on a laboratory roll mill (\emptyset 150 x 300 mm) at 20 rpm with a batch size of approx. 600 cm³. The mixing times were adjusted according to the incorporation characteristics of the filers, and were registered. The curing time in all cases was t₉₀ + 10 % at 180 °C in an electrically heated press (*Fig. 7*).

	Preparation and Curing of the Compound	HOFFMANN
INTRODUCTION	• Mixing	
EXPERIMENTAL	Open mill Ø 150 x 300 mm	
RESULTS	Batch volume: approx. 600 cm³	
SUMMARY	Temperature: 50 °C	
	Mixing time: approx. 20 min.	
	• Curing	
	Press, 180 °C, t ₉₀ + 10 %	
C. C. C. C.	VM-2/0311/02.2012	

Fig. 7

3 <u>Results</u>

3.1 Mooney Viscosity und Mooney Scorch Time

The reduction of the petroleum based raw materials caused a slight decrease of the Mooney viscosity (*Fig. 8*).

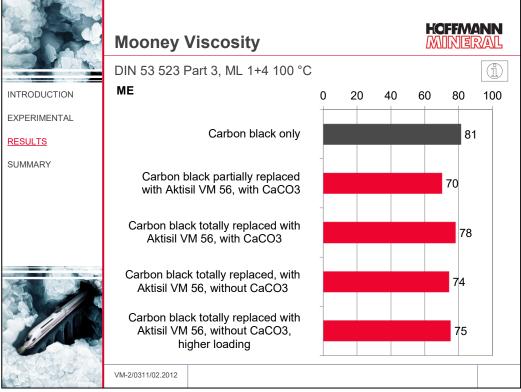
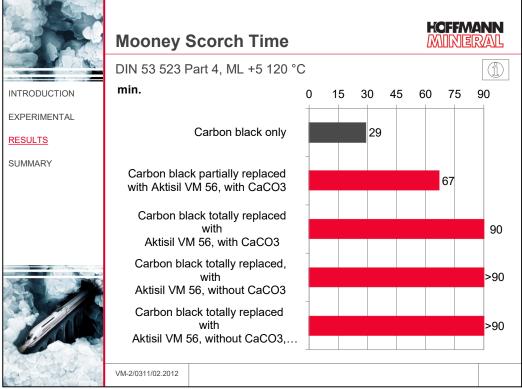


Fig. 8

The Mooney scorch time, an index for the onset of cure during processing, shows a marked increase with an increasing portion of mineral fillers. This means that the risk of scorch (onset of cure) during the processing steps is minimized (*Fig. 9*).





3.2 Curing Properties

With an increasing loading of mineral fillers, the minimum torque will slightly go down, while the torque maximum shows a certain increase. This result indicates a better yield of cure (*Fig. 10 and 11*).

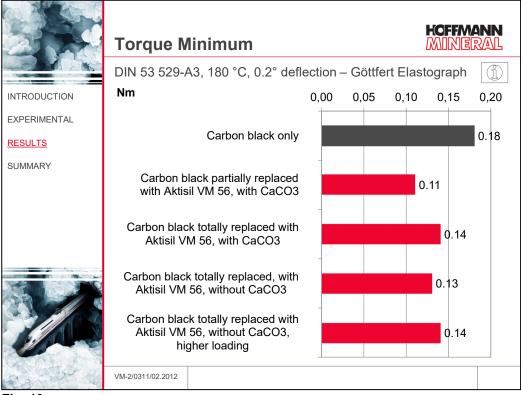


Fig. 10

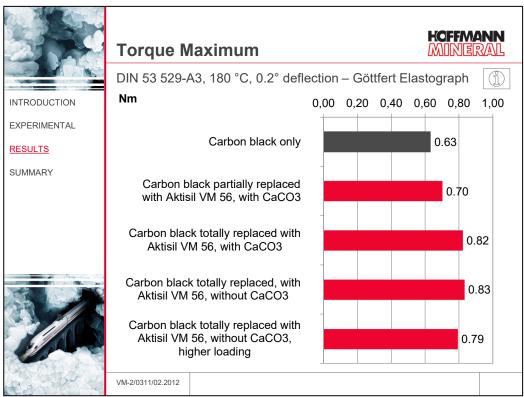


Fig. 11

The conversion time t_{90} will somewhat increase with a higher portion of mineral fillers (Fig. 12).

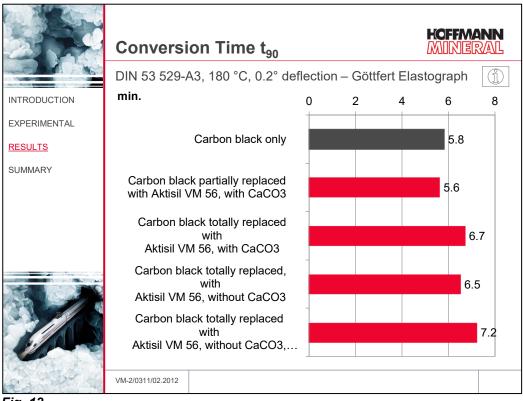


Fig. 12

3.3 Mechanical Properties

All compounds were adjusted to a Shore A hardness of approx. 65 (Fig. 13).

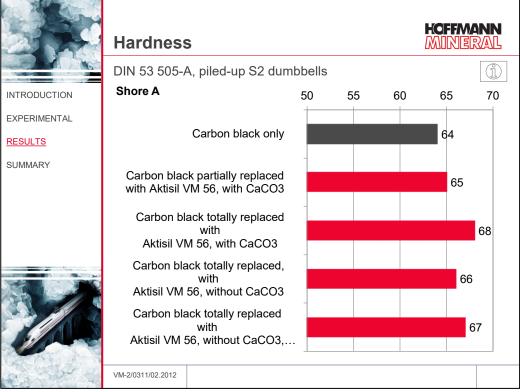


Fig. 13

The guideline for the mechanical properties are the German standards DIN 7863 and RAL-GZ 716/1. The DIN 7863 serve differentiate with the tensile strength between window and application of fronts. Even with higher mineral filler loading all requirements as specified in the standards are still met, while they are clearly exceeded in window application (*Fig. 14*).

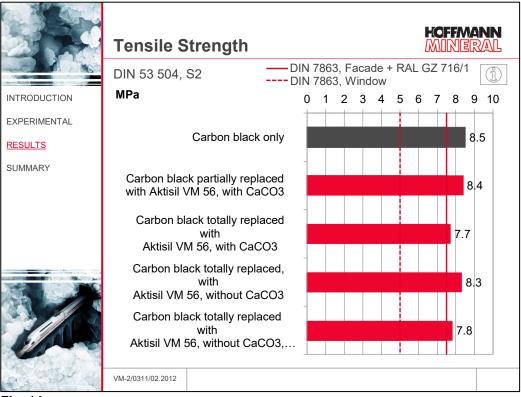


Fig. 14

The elongation at break shows a decrease with increasing amounts of mineral filler, but still remains above the limits of the DIN and RAL standard (*Fig. 15*).

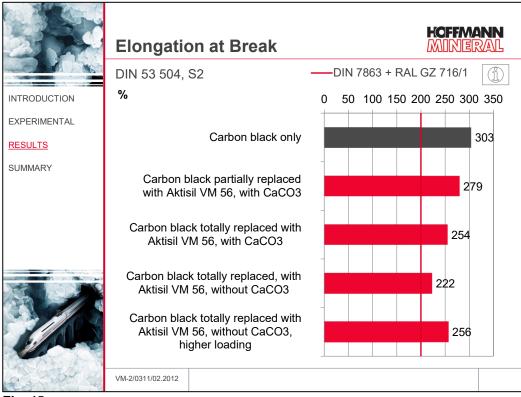


Fig. 15

The higher the portion of mineral filler the higher the tensile modulus at 100 % elongation is (*Fig. 16*).

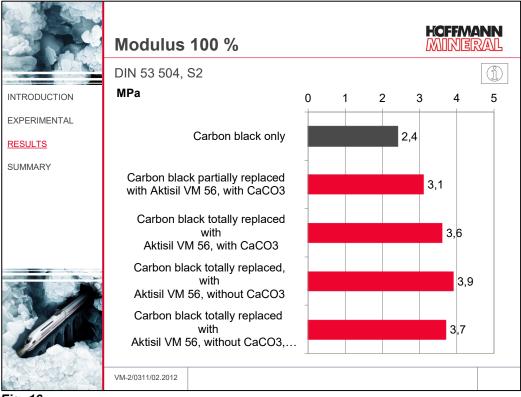


Fig. 16

With the mineral fillers, the compression set at high temperature remains unchanged or is slightly improved. Only in the last formulation variant with the increased loading, the compression set comes out somewhat increased. But all of them still remain within the specification of the DIN and RAL standard (*Fig. 17*).

	Compres	sion Set					
	DIN 53 517 I, 24 h / 100 °C			——DIN 7863 + RAL GZ 716/1			
INTRODUCTION	%		0	10	20	30	40
EXPERIMENTAL							
RESULTS		Carbon black only		12	2		
SUMMARY		k partially replaced /M 56, with CaCO3		10			
		ack totally replaced with I 56, with CaCO3		1	3		
		ick totally replaced, with 56, without CaCO3		11			
		ack totally replaced with 56, without CaCO3,			15		
100 ×	VM-2/0311/02.2012						



The results at 23 °C are partially already close to the limit of the RAL standard, even if all formulations meet the requirement of RAL-GZ 716/1 regarding to the compression set at ambient temperature.

The partly or total replacement of Carbon black with mineral fillers leads to a markedly lower compression set. Despite the higher filler loading of the last compound variant it achieves the compression set level of the straight carbon black formulation (*Fig. 18*).

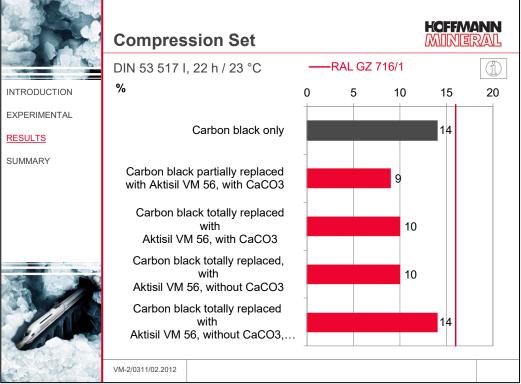


Fig. 18

3.4 Response to low Temperature

Straight carbon black meets the requirement of the standards just borderline. Here a higher portion of mineral filler has a very positive effect on the hardness change at low temperature, thus complying the standards more safely (*Fig. 19*).

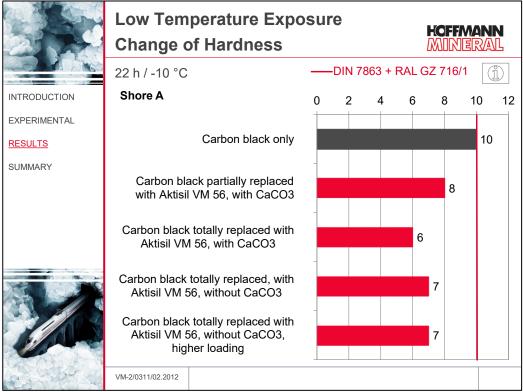


Fig. 19

4 <u>Summary</u>

- Aktisil VM 56 allows to meet the essential requirements of the DIN 7863 and RAL-GZ 716/1.
- According to the circumstances, a refining optimization approach such as a reduction of the peroxide concentration, can be useful.
- This way, it is possible to considerably decrease the portion of petroleum based raw materials in the compound, which leads to more safety in planning of the raw material costs.
- On the technical side, according to the formulation used the following results can be attained:
 - lower viscosity
 - increased scorch safety
 - increased tensile moduli
 - improved compression set
 - lower change of hardness at -10 °C

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